# peciale

LE TECNOLOGIE DI CARBON CAPTURE AND STORAGE

## Techno-economic feasibility study and environmental performance analysis of a power generation plant with CCS system

In order to increase Italian national energy security (partially releasing energy production from imported primary sources) and to re-launch the economy in the Sulcis area (South-West Sardinia, Italy), the Italian Government and the Sardinian Regional Administration are strongly interested in the development of an industrial project for the construction of a 300-450 MWe power generation plant, equipped with a demonstration carbon capture and storage (CCS) system. The plant has been conceived to operate in close integration with a sub-bituminous coal mine in the Sulcis area, where the only Italian coal basin is located.

In this context, Sotacarbo is engaged in the development of a detailed study with the end to evaluate the feasibility of this project and to define the best plant configuration and operating parameters.

This paper shortly describes a portion of this study, in which a preliminary comparative analysis (from the technical, economical and environmental points of view) of all the technical alternatives allows to select the best plant configuration: an ultra supercritical pulverized coal combustion (USPCC) plant, equipped with a SNOXTM section for the combined removal of SOx and NOx and with a partial capture of CO<sub>2</sub>.

Due to the potential unreliability of some assumption and to the impossibility to estimate with accuracy the future trend of some operating parameters, a sensitivity analysis has been assessed in order to evaluate the effects of these assumptions, with a subsequent reduction of the investment risk



### Studio di fattibilità tecnico-economica ed analisi dell'impatto ambientale di un impianto di generazione di potenza basato sulla tecnologia di cattura post-combustione della CO2

Al fine di incrementare la sicurezza energetica nazionale e rilanciare l'economia dell'area del Sulcis, il Governo e la Regione Sardegna sono fortemente interessati allo sviluppo di un progetto dimostrativo delle tecnologie CCS, relativo ad un impianto di generazione di potenza da 300-450 MWe, integrato al sito di stoccaggio in una miniera di carbone sub-bituminoso nell'area del Sulcis. L'analisi comparativa delle diverse possibili alternative permette di individuare in un impianto al polverino di carbone Ultra Super Critico, equipaggiato con sistemi DeNOx, DeSOx e con parziale cattura della CO2 con solventi, come la soluzione tecnologicamente ed economicamente più conveniente

Eusebio Loria, Alberto Pettinau, Carlo Amorino, Mario Porcu

#### Introduction

Power generation in Italy is based for about 75% on fossil fuels, with an annual  $CO_2$  emission of about 430 Mt [1]. Moreover, coal consumption amounts to about 13.4 million of tones of oil equivalent (toe), corresponding to only 8.8% of the global consumption of fossil fuels [2]. This involves a very high cost of electrical energy and a low energy security.

This justify the strong interest of the Italian Government and the Sardinian Regional Administration in the development of the only Italian coal basin, located in the Sulcis area, in South-West Sardinia. Since 1994, a series of national laws has been promulgated in order to promote the construction of a Sulcis coal feed power generation plant capable to enhance the national energy security and the weak and poor economy of the Sulcis area. In particular, the Italian law n. 99 (July 23, 2009) requires the construction of a 300-450 MWe power gener-

■ Eusebio Loria, Alberto Pettinau, Carlo Amorino, Mario Porcu

ation plant strictly integrated with the Sulcis coal mine and feed with at least 50% (lower heating value - LHV basis) of local coal (characterized by a very high sulphur content, of about 6-7% in weight), which can be assimilated to renewable sources as for the access to the incentives for the selling of the electric energy. Moreover, the plant must be equipped with a demonstration carbon capture and storage (CCS) section.

In this scenario, Sotacarbo (in cooperation with ENEA, the Italian National Agency for Energy and Environment) is currently supporting the Italian Ministry of Economical Development and the Sardinian Regional Administration to define the guidelines for the development of such a project.

This paper presents a hint about the preliminary results of a technical, economical and environmental analysis which has been carried out in order to assess the feasibility of this project. In particular, a series of technical and environmental cases led the choice of two plant configuration, based on IGCC (integrated gasification combined cycle) and USPCC (ultra supercritical pulverized coal combustion) technologies, respectively. For both these plant configurations, a preliminary economical analysis suggested that USPCC is most profitable than IGCC, and a more detailed prefeasibility study has been carried out for the ultra supercritical plant configuration, in order to determine the best plant size and the main operating conditions, together with the analysis of the investment on the basis of the main economical parameters.

#### Power generation plant configuration

A preliminary analysis of the state-of-the-art of the technologies currently available for power generation in the Sulcis area through a medium-scale (300-450 MWe) power plant initially indicated four main potential technologies for power generation section: ultra supercritical pulverized coal combustion (USPCC), supercritical circulating fluidized bed combustion (CF-BC), supercritical pressurized fluidized bed combustion (PFBC) and integrated gasification combined cycle (IGCC), the latter based on a dry-feed Shell gasification technology.

In particular, for the three combustion-based technologies, two different flue gas treatment processes have been considered: a conventional flue gas desulphurization (FGD) system for SOx removal with a selective catalytic reduction (SCR) system for NOx removal or an advanced SNOX<sup>TM</sup> system (licensed by Haldor Topsøe) for a combined separation of nitrogen and sulphur oxides. On the other hand, a Selexol<sup>TM</sup> (licensed by UOP LLC.) system for sulphur compounds removal and a Claus/SCOT system for sulphur recovery and tail gas treatment have been selected for the IGCC plant.

#### Choice of plant configuration

A preliminary analysis of the environmental performance of each plant configuration restricts the choice to USPCC plant with SNOXTM system and IGCC. As a matter of fact, all the considered plant configurations allow to achieve very low emissions of SOx, NOx and particulate (20-100 mg/Nm<sup>3</sup> for both SOx and NOx and about 5 mg/Nm3 for particulate), whereas the solid and liquid wastes production is strongly different. In particular, both the fluidized bed combustion processes (CFBC and PFBC) involve a large amount of not recoverable solid residues; moreover, flue gas treatment with FGD process involves a high production of liquid and solid wastes. This high residues production does not respect the recommendations included in the above cited law n. 99/2009.

On the other hand, USPCC plant equipped with SNOXTM system and IGCC configurations can be considered near zero emissions plant: as a matter of fact, solid residues (bottom ash or slag) are inert and recoverable for both plant configurations [3], the production of waste liquids is negligible and the main byproducts (sulphuric acid from SNOX<sup>TM</sup> process or solid sulphur from Claus process) are characterized by a high commercial value [4].

A preliminary economical analysis (which considers both plant configuration equipped with CCS system) indicates USPCC technology as the most promising for this specific application (with a plant scale between 300 and 450 MWe). As a matter of facts, with respect to IGCC plant, USPCC allows a lower capital cost and a higher plant availability, with a subsequent higher global profit.

#### Selected power generation technology

The selected power generation plant is based on an ultra supercritical boiler which operates at about 25-28 MPa and 580-600 °C (steam superheater process conditions) and allows a very high efficiency of the combustion phase and of the steam cycle [5], whereas the bottom ash is inert and it could be permanently stored in the exhausted seams of the coal mine or recovered as building material [6].

Flue gas is sent to a fabric filter, which operates the particulate separation, and to the SNOXTM section, in which the sulphur oxides contained in the flue gas are removed and recovered as commercial grade sulphuric acid, whereas NOx is reduced to N2. This system does not consume water or other materials, except for the ammonia used for the catalytic NOx reduction; more-



over, it does not generate any secondary source of pollution, such as waste water, slurries or solids [7-9].

The overall plant efficiency, considering its basis configuration (without CCS), is 45.0% [10].

#### Carbon capture section

As mentioned, the considered power generation plant needs to be equipped with a demonstration carbon capture and storage system.

A post-combustion CO<sub>2</sub> absorption system based on an aqueous solution of monoethanolamine (MEA) has been considered in this study. This system treats the plant flue gas and operates chemical absorption of carbon dioxide at atmospheric pressure and at about 45-50 °C, with a CO<sub>2</sub> removal efficiency of about 90%

The introduction of CCS system involves a significant decreasing (typically 8-12 percentage points) of the overall plant efficiency, due to the high energy consumption of the process; in particular, solvent regeneration requires a significant amount of steam (ex-

tracted from the steam turbine, with a subsequent reduction of power output), whereas CO, compression requires a high power absorption [12-13].

#### Carbon dioxide geological storage

As for the CO<sub>2</sub> geological storage, two different technologies have been considered in this analysis: the storage in saline aguifers below the Sulcis coal basin and the storage through ECBM (enhanced coal bed methane) technique.

The storage in the saline aquifers takes place injecting compressed CO2 at a depth of about 1000-1200 m in the southern area of the Sulcis coal basin, where the aquifers are located. In the same area of the basin, the ECBM technique should be tested at a depth of about 800-1.000 m; in particular, compressed CO, injected into the unminable coal seams is adsorbed by the mineral material, thus displacing methane.

Preliminary studies show that the Sulcis coal basin is capable for the application of both carbon sequestration technologies due to a series of cases such as the

	0Plant configurations		
	300 MWe plant (total capture)	450 MWe plant (total capture)	450 MWe plant (partial capture)
Gross thermal input (MW)	857	1285	1173
Overall plant efficiency (LHV basis)	35.0%	35.0%	38.0%
Basis plant efficiency (without CCS)	45.0%	45.0%	45.0%
Plant availability (hours/year)	7000	7000	7000
Net power output (GWh/year)	2100	3150	3150
Flue gas production (Nm3/hour)	953 585	1 428 539	1 374 447
Percentage of flue gas treated by CCS system	100%	100%	67%
Percentage of Sulcis coal (LHV basis(a))	50%	50%	50%
Sulcis coal consumption (Mt/year)	0.518	0.777	0.710
Imported coal consumption (Mt/year)	0.435	0.653	0.596
SOx emissions (b) (mg/Nm3 – t/year)	40–200	40–300	40–290
NOx emissions (b) (mg/Nm3 - t/year)	20–133	20–200	20–192
Particulate emissions (b) (mg/Nm3 - t/year)	5 – 33	5 – 50	5 – 48
CO <sub>2</sub> capture efficiency	90.0%	90.0%	90.0%
Produced CO <sub>2</sub> (Mt/year)	2.065	3.097	2.827
Emitted CO <sub>2</sub> (Mt/year)	0.206	0.310	0.969

Notes: (a) A LHVof 20.83 MJ/kg and 24.79 MJ/kg has been considered for Sulcis and imported coal, respectively. (b) Specific emissions of SOx, NOx and particulate are referred to an oxygen concentration in flue gas of 6% in volume.

TABLE 1 Main technical assumption for the selected plant configurations Fonte: Sotacarbo

extension of the saline aquifers, the homogeneity of the reservoir, the rank of the sub-bituminous Sulcis coal, the permeability of the coal bed and the presence of a natural cap-rock which allows a permanent segregation [6, 14].

#### Assumptions on plant configuration and size

As previously mentioned, the Italian law n. 99/2009 recommends a plant scale between 300 and 450 MWe. In this study, both these extreme sizes have been considered for the CO<sub>2</sub>-free plant. Moreover, a third hybrid configuration considers a power generation plant which produce 450 MWe and with the CCS system designed to treat only a portion of flue gas (corresponding to that produced by a hypothetical 300 MWe CO<sub>o</sub>free power generation plant). This third possibility could represent a good compromise, from the economical point of view, considering that the aim of CCS system is to demonstrate the feasibility of the technology and the corresponding cost could be partially supported by the Italian Government.

Table 1 shows the main technical assumptions of the three mentioned plants. In particular, a plant availability of 7000 hours per year has been considered for each case. This value has been precautionary assumed lower than that corresponding to the state-ofthe-art (typically 7600-8000 h/yr.) taking into account the demonstration nature of the CCS system and the subsequent implications in the management of the power generation plant (which could operate even during the shut-down of the capture system, with a lower fuel consumption).

#### **Economical and financial assumption**

The economical and financial analysis here reported for the three considered plant configurations takes into account every cost (mainly capital and operating costs for power generation and for CO2 capture and storage) and profit (for the selling of electrical energy and CO<sub>2</sub> assigned amount units).

#### Capital costs

The assessment of the plant capital cost considers the overall plant construction and the adjustment of the infrastructure. Capital cost estimation for each plant configuration is shown in table 2 [6, 10]. In the financial assessment, the investment has been considered with its distribution during the construction period of four years (since 2012 to 2015). In particular, 24% of the capital cost is invested during the first year of construction, whereas 39%, 32% and 5% are invested during the following three years, respectively.

A typical detailed cost distribution for plant construction, recently proposed by the U.S. Department of Energy [5], is shown in table 3. The total investment cost is composed by the sum of equipment costs, material costs, direct and indirect labour, engineering costs and other capital costs. As for the equipments, the most significant contribute in the total plant cost comes from the ultrasupercritical boiler and for the CO, capture and compression system (which globally represents about 52.3% of the total capital cost).

Capital cost affects significantly the behaviour of the annual cash flow. For this reason, this cost has been considered with its financial amortization schedule. Table 4 shows the main economic parameters assumed in this analysis. In particular, 80% of the capital costs has been assumed funded by the banks, with a

	Capital costs (M/)			
	300 MWe CCS 100%	450 MWe CCS 100%	450 MWe CCS 67%	
Power generation plant	1090.9	1380.0	1254.5	
-"basis" configuration	736.4	988.2	900.0	
-CCS system	354.5	391.8	354.5	
Other capital costs (a)	87.3	110.4	100.4	
Contingencies (b)	21.8	27.6	25.1	
TOTAL	1200.0	1518.0	1380.0	

Notes: (a) 8% of the plant cost; they include engineering, start-up, spare parts, royalties and working capital. (b) 2% of the plant cost.

Capital costs Fonte: Sotacarbo



	Equipm.	Material	Labur (direct)	Labour (indir.)	Engin. &fee	Other costs	TOTAL
Coal/sorbent handling	1.25%	0.34%	0.75%	0.00%	0.21%	0.38%	2.93%
Coal/sorbent prepar. and feed	0.85%	0.05%	0.22%	0.00%	0.10%	0.18%	1.10%
Feedwater and misc. BoP	3.42%	0.00%	1.61%	0.00%	0.46%	0.90%	6.40%
PC boiler and accessories	12.23%	0.00%	6.86%	0.00%	1.86%	2.09%	23.04%
Flue gas cleanup	6.31%	0.00%	2.15%	0.00%	0.81%	0.93%	10.20%
CO <sub>2</sub> removal and compr.	14.69%	0.00%	4.48%	0.00%	1.83%	8.26%	29.26%
Ductwork and stack	1.09%	0.06%	0.74%	0.00%	0.17%	0.27%	2.34%
Steam turbine generator	5.25%	0.07%	1.43%	0.00%	0.62%	0.87%	8.25%
Cooling water system	1.29%	0.62%	1.15%	0.00%	0.29%	0.45%	3.81%
Ash/spent sorbent handling	0.33%	0.01%	0.44%	0.00%	0.08%	0.09%	0.94%
Accessory electric plant	1.57%	0.67%	1.88%	0.00%	0.36%	0.56%	5.05%
Instrumentation and control	0.63%	0.00%	0.63%	0.00%	0.11%	0.24%	1.61%
Improvements to site	0.21%	0.12%	0.42%	0.00%	0.07%	0.16%	0.98%
Buildings and structures	0.00%	1.55%	1.47%	0.00%	0.27%	0.49%	3.78%
TOTAL	49.14%	3.48%	24.24%	0.00%	7.26%	15.89%	100.0%

TABLE 3 Power generation plant cost distribution<sup>[5]</sup>
Fonte: Sotacarbo

Plant construction period (a) (years)	4
Plant operating life (b) (years)	21
During of financial amortization (years)	10
Annual discount rate (c)	10%
Annual inflation rate	2%
Plant value at the end of operating life (M)	0.00
Percentage of external funding	80%

Notes: (a) Since 2012 to 2015. (b) Since 2016 to 2037. (c) Source: Dominichini, 2009 [10].

TABLE 4 Main financial assumptions
Fonte: Sotacarbo

discount rate of 10% (precautionary); the annual rate of the capital cost (which is the addition of the constant capital share and the decreasing annual interest and amounts to 258 M $\in$ , with reference to the year 2016 and to the  $\rm CO_2$ -free 450 MWe configuration) has been calculated according with the straight-line method.

#### Overall operating costs

The overall operating cost of the power generation plant considers the purchasing of Sulcis and imported coal (65  $\in$ /t and 60  $\in$ /t, respectively, including transport and delivery), the operation and maintenance (O&M) of the plant, together with the cost for material handling and taxes.

In particular, the operating and maintenance cost includes all the costs for conduction and maintenance of the power generation plant and, in particular, the cost of labour, the day-by-day maintenance, the cost for spare parts and so on.

The evaluation of these costs has been carried out on the basis of a previous assessment [6], adjusting every cost component in order to consider the different plant configuration and scale. All these costs have been considered with an annual increasing of 2% in order to take into account the current trend of the price. This evaluation does not consider the cost for ash handling and disposal into the exhausted seams of the coal mine; it has been assumed that this cost is fully compensated by the selling of the by-products (sulphuric acid from SNOX<sup>TM</sup> process) [6].

#### Profit for CO2 assigned amount units

In this study, the profit for the selling of the CO2 assigned amount units (AAUs) has been considered, according with the Emissions Trading System (ETS), for the evaluation of the annual cash flow. In particular, the CO<sub>2</sub> emission limit has been calculated according with the last available Italian national allocation plan (NAP) for the period 2008-2012, with the assumption that the same value will be constant during all the plant operating life. In particular, for the considered plant configurations, the emission limit amounts to 1603 Mt/yr. for the 300 MWe plant, to 2407 Mt/yr. for the CO<sub>2</sub>-free 450 MWe plant and to 2198 Mt/yr. for the 450 MWe configuration with partial capture.

Moreover, an averaged value of 25 €/t has been considered for the CO, AAUs during all the plant operating life. Globally, the profits for the selling of the AAUs amounts to 35.12 M€/yr. for the CO<sub>2</sub>-free 300 MWe plant, to 52.70 M€/yr. for the CO<sub>2</sub>-free 450 MWe plant and to 30.90 M€/yr. for the 450 MWe plant with partial capture.

It is important to underline that these assumption are arbitrary, being impossible to preview the future trend of CO2 value. Therefore, a sensitivity analysis has been carried out in order to assess the effects of this parameter.

#### Profit for electrical energy production

The electrical energy produced by the power generation plant is sold to the national electric grid (and, in particular, to GSE SpA, the Italian national company for the management of the electrical services) and represents the main profit of the industrial application. Its cost has been calculated with reference to the Italian ordinance CIP 6/1992 [15], which defines the price of electricity on the basis of the "avoided costs". Moreover, for the first eight years of the plant operat-

	Price <sup>(a)</sup> (c€/kWh)
Overall avoided cost	8.585
- plant avoided cost	2.295
- operating avoided cost	0.790
- fuel avoided cost	5.500
Incentive (b)	7.025
Overall price of electrical energy	15.610

Notes: (a) Referred to the first year of plant operation (2016). (b) Only for the first eight years of operation (2016-2023)

Price of electrical energy Fonte: Sotacarbo

ing life (since 2016 to 2023), GSE pays an extra incentive for energy selling, according with the Italian law d.p.r. 28/01/94. The price of the electrical energy sold to the national grid is shown in table 5, with reference to the first year of the plant operating life (2016).

After the eighth year (since 2024), when the payment of incentive is suspended, a slight charge of the energy price (initially 0.85 c€/kWh) must be also considered, according with the Italian law d.p.r. 28/01/94.

Every component of the overall price of the electrical energy (except for the fuel avoided cost, according with ordinance CIP6) has been calculated for every year of the plant operating life, considering an annual increasing of 2%.

#### Cost for CO2 geological storage

This study considers a CO<sub>2</sub> geological storage through injection in the saline aquifers under the coal mine. In particular, carbon dioxide is dried and compressed, at about 10 MPa (and, in any case, higher than the critical pressure: 7.5 MPa) [16-17], and send, through a pipeline, to the injection wells, located about 20-30 km far from the power generation plant. The overall specific cost for CO2 compression, transport and injection has been considered constant for each year (except for the annual increasing of 2% due to inflation); moreover, they include both capital and operating costs, except for CO2 compression (which capital cost is included in the initial investment for the capture section).



The compression technology, based on a multistage intercooled compressor, is quite mature and does not need further development for applications with  $CO_2$ , except for the optimization of its integrations with the specific power plant [18]. A compression cost of 0.75 c $\in$  per kilogram of  $CO_2$  [19] has been assumed. On the other and, pipelining  $CO_2$  is a well-estabilished technology, which uses the normal gas construction methods [20-21]. A transport cost of 2.5 c $\in$ /t km, referred to onshore pipeline [22], has been assumed. Finally, an injection cost of 3.4 c//t has been considered for the carbon sequestration in saline aquifers.

#### Results and discussion

The economical and financial assessment of the investment has been carried out by the evaluation, year by year, of the effective and actualized cash flow, the latter referred to the first year of the project financing phase (2012). A comparison between the different plant solution has been carried out with reference to the typical economical indicators, i.e. net present value, internal rate of return and payback time.

In particular, the net present value (NPV) is defined as the sum of the present values of the individual cash flows.

The internal rate of return (IRR) is the value of the dis-

	300 MWe CCS 100%	450 MWe CCS 100%	450 MWe CCS 67%
Net present value (M/)	-197.2	158.3	332.4
Internal rate of return (%)	8.27	11.03	12.31
Payback time (a) (years)	-	18	14
Cost of electricity (b) (c€/kWh)	8.98	7.60	7.31
CO <sub>2</sub> separation cost (€/t)	29.34	24.69	29.35
Cost of avoided CO <sub>2</sub> (b) (€/t)	17.36	12.46	15.28

Notes: (a) Including construction period. (b) The assessment considers a cost of AAUs of 25 //t.

TABLE 6 Comparison of the main economical results Fonte: Sotacarbo count rate that makes the net present value of all cash flows equal to zero, whereas payback time (PBT) is defined as the period of time required for the return on the investment (based on actualized cash flows).

Moreover, in order to quantify the economical plant performance, the cost of electricity, of  $\mathrm{CO}_2$  separation and of "avoided  $\mathrm{CO}_2$ " have been also determined. In particular, the cost of electricity (CoE, in  $\mathrm{c} \in /\mathrm{kWh}$ ) is the ratio between all the plant cost (capital and operating, including fuel) during the full duration of the project and the overall electrical energy produced during the same period. In parallel,  $\mathrm{CO}_2$  separation cost is the ratio between the overall (capital and operating) cost of CCS (capture, compression, transport and injection) and the whole amount of stored  $\mathrm{CO}_2$ , during all the project life. Finally, the cost of avoided  $\mathrm{CO}_2$  can be defined as:

$$Ca = (CoE_{ccs} - CoE_{basis}) / (e_{basis} - e_{ccs})$$
 (1)

where CoE is the previously defined cost of electricity and e is the CO<sub>2</sub> specific emission (in kg/kWh) in both basis and CCS configuration; the subscript CCS indicates the assumed plant configuration, whereas the subscript basis indicates the corresponding configuration without CCS, both considered with the same thermal input. Table 6 shows a synthesis of the main results of the comparative economical analysis expressed on the basis of the above defined parameters. As expected, the investment for a 300 MWe CO<sub>2</sub>-free plant appears not feasible from the economic point of view; as a matter of fact, the small plant scale (and its subsequent high specific cost, in €/kWe) does not allow to obtain a positive NPV. The 450 MWe plant with partial capture is significantly more convenient (higher NPV and a moderate value of payback) than the corresponding CO<sub>2</sub>-free configuration. Moreover, with reference to the 450 MWe plant scale, the configuration with partial capture involves a higher CO, emission, and a subsequent higher cost of avoided CO2, with respect to the CO2-free unit. The high value of the internal rate of return (except for the 300 MWe configuration) indicates a secure investment, which remains profitable even if the discount rate (which, in this analysis, has been prudentially overestimated) increases.

It is important to notice that the  $CO_2$  separation cost here determined corresponds to the typical values reported in the scientific literature, between 15 and 30  $\[ \in \] /t^{[23]}$ .

#### Sensitivity analysis

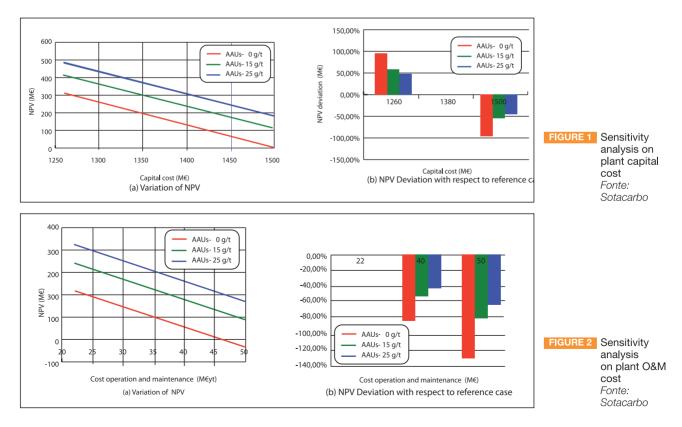
Some of the parameters assumed in this study are affected by an uncertainty, being determined by a large series of key factors which are impossible to foresee. Therefore, in order to assure a security of the potential investment, the effects of the variation of these parameters on the main economical indicators (the results here reported are mainly referred to the net present value) has been evaluated. The results here reported are referred to the 450 MWe power generation plant

with partial  $CO_2$  capture and sequestration, applied to 67% of produced flue gas; moreover, three different costs of  $CO_2$  AAUs have been considered:  $25 \in /t$  (reference case, which represents the most probable scenario in a short-term future),  $15 \in /t$  (current value) and  $0 \in /t$  (a precautionary assumption).

#### Sensitivity analysis on plant capital cost

A detailed value of the plant capital costs can be only evaluated as the results of the detailed plant design. In this preliminary phase, it has been assumed in line with previous evaluation coming from the recent scientific literature.

Figure 1 shows, for three different values of the  $\rm CO_2$  AAUs, the linear variation of NPV by varying the capital cost between 1260 (a future scenario, when the technology will be industrially mature) and 1500 M $\in$  (precautionary case). In particular, the behaviours of NPV have been presented (figure 1.a) together with





the maximum values of deviation (figure 1.b) with respect to reference capital cost (1380 M $\in$ ).

As expected, an increasing capital cost involves a significant reduction of the net present value (this variation is particularly significant when the cost of  $CO_2$  AAUs is low). On the other hand, cost of electricity raises from 7.18  $\[ \in \]$ /t (for a capital cost of 1260 M $\[ \in \]$ ) to 7.74 (for a capital cost of 1500 M $\[ \in \]$ ). In any case, in all the considered range of variation, the investment remains profitable.

Sensitivity analysis on plant operating and maintenance cost

The reference case considered in this work includes an operating and maintenance (O&M) cost of about 22 M $\in$  per year (referred to the first year of plant operating life); this value is fully consistent with that reported in the scientific literature. In any case, it depends by a series of technical and social aspects such as costs of labour, equipments, spare parts and so on. As shown in figure 2, a raise of O&M costs (up to 50 M $\in$ /yr) involves a significant linear reduction (about 60%) of the net preset value and a corresponding increasing (14.6%, up to 9.4 c $\in$ /kWh) of the cost of electricity. Even in this case, this variation is particularly significant when the cost of CO<sub>2</sub> AAUs is low.

Sensitivity analysis on costs for  $CO_2$  geological storage The reference case of this study considers an overall cost for  $CO_2$  storage (including compression, transport and injection) of 3.4 M $\in$  for the first year of plant operating life (with an annual increasing of 2%). This value is referred to carbon dioxide geological storage in the saline aquifers located under the Sulcis coal mine, at a depth of 800-1000 m.

As mentioned, the possibility to operate  $\mathrm{CO}_2$  storage through ECBM (enhanced coal bed methane technology) is also under investigation, due to the closeness of the considered power plant to the Sulcis coal basin. In particular,  $\mathrm{CO}_2$  injected into coal seams displaces methane, thereby enhancing coal-bed methane recovery [24]. As for this technology, a typical cost of 30 M $\in$  per year (with the hypothesis that the extraction of methane is negligible) or lower (depending by the profits for methane selling) can be considered.

As shown in figure 3, this cost strongly influences the NPV, which is null when the cost of  $CO_2$  storage is about  $27\text{-}28 \in /t$ . In these case, the investment became unprofitable. Due to the demonstration nature of the CCS section, a plausible scenario could consists in a combined storage in which about 70% of captured  $CO_2$  is stored in saline aquifers, whereas the remaining 30% is injected in the unminable coal seams, with an annual overall cost of about 15 M $\in$  (referred to the first year of plant operating life). In this scenario, NPV decreases to 171.5 M $\in$  (-48.3%), whereas CoE raises up to 8.3 c $\in$ /kWh (11.3%). Moreover, cost of avoided  $CO_2$  increases from 16.6 to 21.5  $\in$ /t whereas cost of  $CO_2$  separation raises from 29.3 to 43.6  $\in$ /t

Sensitivity analysis on other significant parameters

The influence of other significant parameters on the

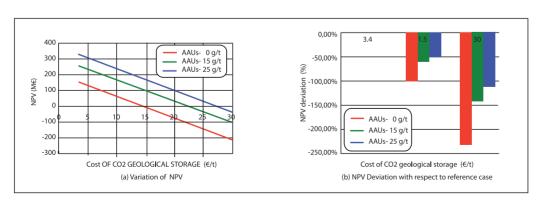


FIGURE 3 Sensitivity
analysis
on costs for
CO<sub>2</sub> geological
storage
Fonte:
Sotacarbo

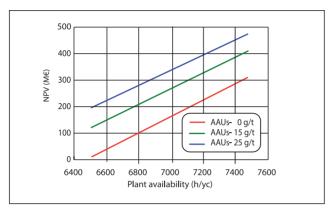


FIGURE 4 Sensitivity analysis on plant annual availability
Fonte: Sotacarbo

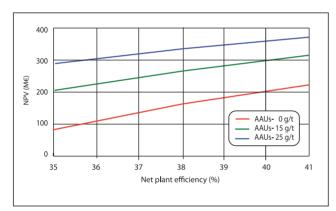


FIGURE 5 Sensitivity analysis on plant efficiency
Fonte: Sotacarbo

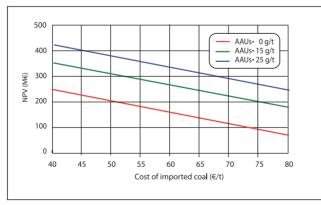


FIGURE 6 Sensitivity analysis on the cost of imported coal Fonte: Sotacarbo

economic performance of the investment has been also assessed. In particular, plant availability significantly influences the annual profit (due to energy selling); an increasing value of this parameters up to 7500 h/yr. involves a raise of NPV (figure 4) of about 42% (92-93% if the cost of AAUs is null), whereas the cost of electricity decreases to 7.28 c€/kWh.

The overall net plant efficiency of a CCS plant is one of the most controversial aspects in the development of this kind of technology. As mentioned above, in this study a net efficiency of 45% (LHV basis) has been considered for the basis configuration; it decreases down to 38% as a consequence of the introduction of the CCS system designed to treat only a portion of flue gas. Considering the reference case, with a cost of AAUs of 25€/t, a variation of the overall plant efficiency between 35 and 41% involves an increasing of the NPV, between 286 and 370 M€ (figure 5), and a subsequent decreasing of CoE from 7.72 to 7.25 c€/kWh.

Finally, the economical performance of the investment is significantly affected by the cost of imported coal. In particular, an increasing of this cost up to  $80 \in /t$  (figure 6) should involve a reduction of the net present value of about 26.8% (about 240 M $\in$ ) and a corresponding increasing of CoE of 6.17% (7.92 c $\in$ /kWh).

#### **Conclusions**

In order to increase Italian energy security (partially releasing energy production from imported primary sources) and to re-launch the economy in the Sulcis area, Sotacarbo is cooperating with national and regional administrations to develop a project for the construction of a power generation plant, equipped with a demonstrating CCS system, strictly integrated with the Sulcis cola mine.

Between all the available technologies, the most profitable plant configuration includes a 450 MWe power generation plant, based on the pulverized coal combustion in an ultra supercritical boiler, equipped with a SNOX<sup>TM</sup> system and a MEA-based post-combustion

CO<sub>2</sub> capture plant which treats about 67% of the plant flue gas (corresponding to an hypothetical 300 MWe CO<sub>2</sub>-free plant).

The analysis here presented takes into account capital (about 1380 M€) and operating costs, together with the profits for the selling of electrical energy and CO, AAUs, according with the international Emissions Trading System. The proposed solution appears significantly profitable, with a net present value of 332 M€; moreover, the high internal rate of return (12.31%) and the relatively low payback time (14 years) assure a good reliability of the investment.

As results from the sensitivity analysis, the evaluation of capital and O&M cost strongly influences the economical performance of the investment, which remains in any case profitable if the cost of CO2 AAUs will remain around 15-25 €/t during the plant operating life. Moreover, the relatively high profit margin allows and suggests to test both the selected CO, sequestration techniques: geological storage in saline aguifers and through ECBM, the latter (which is characterized by a very high operating cost) applied only for a portion (around 20-30%) of captured carbon dioxide.

It is important to specify that this study is only a small portion of a more detailed feasibility analysis which will lead, in its first phase, to the definition of all the main technical and economical parameters of the overall project and, in a second phase, to the development of the plant detailed design.

- International Energy Agency. 2010 key world energy statistics. Available at www.iea.org, 2010.
   British Petroleum. BP statistical review of world energy June 2010.
- Available at www.bp.com, 2010.

  P. de Wit. Driving clean coal forward. Proceedings of the 2007 Gasifi-
- cation Technology conference, San Francisco (California, USA), October 16, 2007.

  A.J. Minchener. Coal gasification for advanced power generation. Fuel,
- vol. 84, 2005, pp. 2222-2235.
- U.S. Department of Energy. Cost and performance baseline for fossil energy plants Volume 1: bituminous coal and natural gas to electricity. Technical report DOE/NETL-2010/1397, available at
- ty. Iechnical report DOE/NETL-2010/1397, available at www.energy.gov, 2010.

  [6] A. Pettinau, C. Puddu, C. Amorino. Technical and economical analysis of a zero-emission power generation plant integrated with a sub-bituminous coal mine in South West Sardinia. Proceedings of the <sup>th</sup> Annual International Pittsburgh Coal Conference, Johannesburg (South Africa), September 10-14, 2007.

  [7] Haldry Topogo, The Topogo SNOVIM technology for algority of the conference of the conferenc
- Haldor Topsøe. The Topsøe SNOX<sup>TM</sup> technology for cleaning of flue gas from combustion of petroleum coke and high sulphur petroleum residues. Available at www.topsoe.com, 2006.
  P. Schoubye, F.E. Jensen. SNOX™ flue gas treatment for boilers burn-
- ing petcock makes petcoke more attractive for power and heat generation. Proceedings of the Petcoke Conference, Orlando (Florida, USA), February 23-27, 2007.
- U.S. Department of Energy. SNOX<sup>TM</sup> flue gas cleaning demonstration project: a DOE assessment. Technical report DOE/NETL-2000/112, available at www.energy.gov, 2000.
- R. Domenichini. Costi di generazione elettrica da impianti con cattura dell'anidride carbonica. Proceedings of the 5th National Conference Zero Emission Rome, Roma (Italy), September 30-October 2,
- [11] G. Pellegrini, R. Strube, G. Manfrida. Comparative study of chemical absorbents in postcombustion CO<sub>2</sub> capture. Energy, vol. 35, 2010,
- absorbents in postcombustion CO<sub>2</sub> capture. Energy, vol. 30, 2010, pp. 851-857.
  [12] G. Lozza, P. Chiesa. Cattura e sequestro della CO<sub>2</sub> nelle centrali a combustibili fossili. Energia, vol. 3, 2007, pp. 84-102.
  [13] T. Harkin, A. Hoadley, B. Hooper. Reducing the energy penalty of CO<sub>2</sub> softeness and compression using pinch applies. Journal of Cleaner
- [13] I. Harkin, A. Hoadley, B. Hooper. Reducing the energy penalty of CO<sub>2</sub> capture and compression using pinch analysis. Journal of Cleaner Production, vol. 18, 2010, pp. 857-866.
  [14] C. Amorino, R. Bencini, R. Cara, D. Cinti, G. Deriu, V. Fandino, A. Giannelli, M. Mazzotti, S. Ottiger, L. Pizzino, R. Pini, F. Quattrocchi, R.G. Sardu, G. Storti, N. Voltattorni. CO<sub>2</sub> geological storage by ECBM techniques in the Sulcis Area (SW Sardinia Region, Italy). Proceedings

- of the 2<sup>nd</sup> International Conference on Clean Coal Technologies for Our Future, Castiadas (Italy), May 10-12, 2005
- [15] Comitato Interministeriale dei Prezzi (CIP). Prezzi dell'energia elettrica relativi a cessione, vettoriamento e produzione per conto dell'Enel, parametri relativi allo scambio e condizioni tecniche generali per l'assimi-
- rametri relativi allo scambio e condizioni tecniche generali per l'assimilabilità a fonte rinnovabile. Ordinance n. 6, 1992.

  [16] K. Michael, A. Golab, V. Shulakova, J. Ennis-King, G. Allinson, S. Sharma, T. Aiken. Geological storage of CO<sub>2</sub> in saline aquifers A review of the experience from existing storage operations. International Journal of Greenhouse Gas Control, vol. 4, 2010, pp. 659-667.

  [17] K. Michael, G. Allinson, A. Golab, S. Sharma, V. Shulakova. CO<sub>2</sub> storage in saline aquifers II Experience from existing storage operations.
- Energy Procedia, vol. 1, 2009, pp. 1973-1980.

  [18] L.M. Romeo, I. Bolea, Y. Lara, J.M. Escosa. Optimization of intercooling compression in CO<sub>2</sub> capture systems. Applied Thermal Engineering, vol. 29, 2009, pp. 1744-1751.
- [19] C. Hendriks, W. Graus, F. van Bergen. Global carbon dioxide storage potential and costs. Ecofys report EEP-02001, Utrecht (The Nether-
- [20] S. Wong, R. Bioletti. Carbon dioxide separation technologies. Alberta Research Council report, available at www.arc.ab.ca, 2002.
- [21] V. Vandeginste, K. Piessens. Pipeline design for a least-cost router ap-
- [21] V. Varideginiste, K. Piessenis. Pipelline design for a least-cost router application for CO<sub>2</sub> transport in the CO<sub>2</sub> sequestration cycle. International Journal of Greenhouse Gas Control, vol. 2, 2008, pp. 571-581.
  [22] B. Metz, O. Davidson. H. de Coninck, M. Loos, L. Meyer. Carbon dioxide capture and storage. IPCC Special Report, ISBN 92-9169-119-4, 2005.
  [23] L. Parker, P. Folger, D.D. Stine. Capturing CO<sub>2</sub> from coal-fired power plants: challenges for a comprehensive strategy. U.S. Congressional Property Capture, proact 3, 75700 englishes between 2010.
- Research Service, report 7-5700, available at www.crs.gov, 2010.

  [24] M. Mazzotti, R. Pini, G. Storti. Enhanced coalbed methane recovery.

  The Journal of Supercritical Fluids, vol. 47, 2009, pp. 619-627.
- [20] S. Wong, R. Bioletti. Carbon dioxide separation technologies. Alberta Research Council report, available at www.arc.ab.ca, 2002.
   [21] V. Vandeginste, K. Piessens. Pipeline design for a least-cost router ap-
- [21] V. Varioeginiste, K. Piesseris. Pipeline design for a least-cost router application for CO<sub>2</sub> transport in the CO<sub>2</sub> sequestration cycle. International Journal of Greenhouse Gas Control, vol. 2, 2008, pp. 571-581.
   [22] B. Metz, O. Davidson. H. de Coninck, M. Loos, L. Meyer. Carbon dioxide capture and storage. IPCC Special Report, ISBN 92-9169-119-4, 2005. 2005.
- [23] L. Parker, P. Folger, D.D. Stine. Capturing CO<sub>2</sub> from coal-fired power plants: challenges for a comprehensive strategy. U.S. Congressional Research Service, report 7-5700, available at www.crs.gov, 2010.
- [24] M. Mazzotti, R. Pini, G. Storti. Enhanced coalbed methane recovery. The Journal of Supercritical Fluids, vol. 47, 2009, pp. 619-627.